

***Limites d'émission de perturbations dans le  
réseau de transport d'Hydro-Québec***

**Version anglaise à la suite de la décision D-2022-020**





# Emission Limits for Disturbances on the Hydro-Québec Transmission System

Decision D-20~~XX-XXX~~

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## 1 DEFINITIONS

Italicized terms in the text are defined below.

### ***asynchronous generator***

The *asynchronous generator* as defined in the *Technical Requirements for the Connection of Generating Stations to the Hydro-Québec Transmission System*, as approved from time to time by the Régie de l'énergie

### ***disturbance***

In this document, the term *disturbance* refers to the power quality *disturbance*.

The power quality *disturbance* corresponds to any phenomenon causing a variation on the voltage or current wave with respect to its amplitude, its frequency, its shape or the symmetry of the three-phase system.

### ***facility***

In this document, the term *facility* refers to any customer facility as defined in the *Technical Requirements for the Connection of Customer Facilities to the Hydro-Québec Transmission System*, as approved from time to time by the Régie de l'énergie, and any generating station as defined in the *Technical Requirements for the Connection of Generating Stations to the Hydro-Québec Transmission System*, as approved from time to time by the Régie de l'énergie, except *facilities* connected to the 735-kV system. *Disturbance* emission limits are set by the *Transmission Provider* on a case-by-case basis for any *facility* connected, or to be connected, to the 735-kV system. In the latter case, the *disturbance* emission limits, set on a case-by-case basis at voltage level 735 kV, will be subject to specific approval from the Régie de l'énergie, and this under Article 73.1 of the *Act respecting the Régie de l'énergie*.

### ***high voltage***

As defined in the *Conditions of Electricity Service*, as approved from time to time by the Régie de l'énergie, nominal phase-to-phase voltage of 44 kV or more.

### ***nominal voltage***

The *nominal voltage* of a system is the phase-to-phase RMS voltage used to designate a system.

The *nominal voltages* ( $U_{nom}$ ) of the *high-voltage Transmission System* are generally as follows: 44 kV, 49 kV, 69 kV, 120 kV, 161 kV, 230 kV, 315 kV and 345 kV.

### ***synchronous generator***

The *synchronous generator* as defined in the *Technical Requirements for the Connection of Generating Stations to the Hydro-Québec Transmission System*, as approved from time to time by the Régie de l'énergie.

### ***system***

The *system* as defined in the *Glossary of Terms and Acronyms used in Reliability Standards* and its modifications as adopted from time to time by the Régie de l'énergie.

For the purpose of calculating the harmonic impedance values of the *system* (in section 7.4.1), the latter also includes the load and all *facilities* connected to the *system*, excluding the *facility* under study.

### ***Transmission Provider***

Hydro-Québec when carrying on electric power transmission activities.

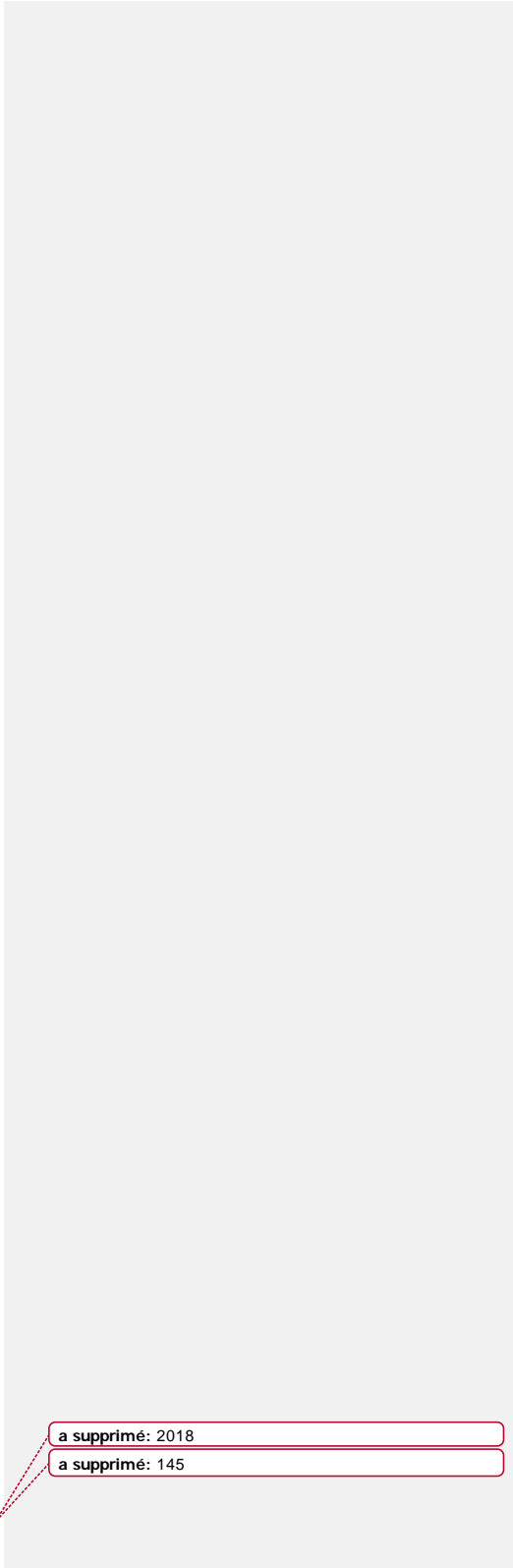
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Emission Limits for Disturbances on the Hydro-Québec Transmission System

**Transmission System**

The *Transmission System* as defined in section 1.49 of the *Hydro-Québec Open Access Transmission Tariff*, as approved from time to time by the Régie de l'énergie.



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## 2 PURPOSE

This document sets out emission limits and emission level assessment methods for power quality *disturbances* on the Hydro-Québec *Transmission System*.

### 2.1 APPLICATION

Emission limits and emission level assessment methods for *disturbances* apply to any *facility* to be connected to the Hydro-Québec *Transmission System*, including the recommissioning of a *facility* that has been completely or partially shut down.

They also apply to any *facility* connected to the *Transmission System* undergoing a modification that might alter its maximum *disturbance* emission levels (e.g., change of *facility* equipment or operating mode).

For an existing *facility* that has not undergone any modification which might alter its maximum *disturbance* emission levels since it was connected to the *Transmission System*, the applicable emission limits are those that were specified initially during *facility* design and set out in the relevant emission study. However, if emission limits and assessment methods set out in this document are less stringent, they may apply to the *facility*.

### 2.2 GENERAL

Emission limits are aimed at ensuring and maintaining the quality of the voltage supplied by the Hydro-Québec Transmission System.

Emission limits are defined for the most common *disturbances*: rapid voltage changes, flicker, load or current unbalance, as well as harmonics and interharmonics.

Emission limits are set on a case-by-case basis for other *disturbances* (e.g., subharmonics, harmonics above 3 kHz and repetitive bursts of harmonic currents).

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a déplacé vers le haut [1]: Emission limits are aimed at ensuring and maintaining the quality of the voltage supplied by the Hydro-Québec Transmission System.¶

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### 3 EMISSION LIMITS

Emission limits are the maximum allowed levels, at the point of evaluation, of *disturbances* generated by a *facility* and propagated on the *Transmission System*.

Emission limits and emission level assessment methods for rapid voltage changes, flicker, load or current unbalances, harmonics and interharmonics are presented in chapters 4, 5, 6, 7 and 8, respectively.

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#### 3.1 EMISSION LEVEL

The emission level represents the contribution of a *facility* to the level of *disturbances* that may be transmitted over the *Transmission System* by the *facility*.

The emission level is assessed according to the methods specified in this document. The emission level must fall below the emission limits set at the point of evaluation.

*Disturbance* levels discussed in this document are measured according to the general approach set out in Appendix B, supplemented by an emission level assessment protocol subject to approval by Hydro-Québec.

#### 3.2 COMPLIANCE WITH EMISSION LIMITS

For each *disturbance*, a simplified assessment or a detailed assessment where appropriate, demonstrating that the *facility* complies with applicable emission limits must be submitted to Hydro-Québec. The required technical information and the general procedure to be followed for assessing emission limit compliance are presented in Appendix A.

##### 3.2.1 Simplified assessment

For each *disturbance*, if the *facility* meets the criteria for simplified assessment, Hydro-Québec must receive a written confirmation in this regard, including the requested data.

##### 3.2.2 Detailed assessment

For each *disturbance*, if the *facility* does not meet the criteria for simplified assessment, Hydro-Québec must receive an emission study and when specified by Hydro-Québec, a report on measurements made in accordance with a protocol approved by Hydro-Québec.

#### 3.3 TRANSMISSION SYSTEM PARAMETERS

The *Transmission System* main parameters indicated below are used as inputs for the assessments.

##### 3.3.1 Point of evaluation

The point of evaluation is a point located on the *high-voltage Transmission System* side where emission levels of the *facility* must be evaluated. This point will generally be the connection point.

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If a *facility* is connected to the *Transmission System* at several connection points, the emission level must be evaluated at all of these connection points.

The *Transmission Provider* may specify another point of evaluation depending on the specific characteristics of the *Transmission System* and on other nearby *facilities* connected to the *Transmission System*.

### 3.3.2 System short-circuit power ( $S_{sc}$ )

The MVA three-phase short-circuit power ( $S_{sc}$ ) of the *system* corresponds to the short-circuit current from the *system* side for a three-phase fault at the point of evaluation for the *facility*.

Theoretical values of  $S_{sc}$  and the corresponding X/R ratio are supplied by the *Transmission Provider* for the point of evaluation, exclusively for the purpose of assessing compliance with emission limits under:

General *system* operating conditions:  $S_{sc, general}$  and  $X/R_{general}$

Occasional *system* operating conditions:  $S_{sc, occasional}$  and  $X/R_{occasional}$

The three-phase short-circuit current ( $I_{sc}$ ) of the *system* is calculated using the three-phase short-circuit power ( $S_{sc}$ ) and the *nominal voltage* ( $U_{nom}$ ) of the *system* at the point of evaluation for the *facility* according to the following formula:  $I_{sc} = S_{sc} / (\sqrt{3} \cdot U_{nom})$ .

### 3.3.3 Reference power ( $S_r$ ) and reference current ( $I_r$ )

The reference power ( $S_r$ ) is the anticipated power of the *facility* in MVA. It is used to determine the emission limits applicable to the *facility* and to assess certain emission levels of the *facility*.

The reference current, also used for this purpose, is defined by the equation ( $I_r = S_r / (\sqrt{3} \cdot U_{nom})$ ), where  $U_{nom}$  is the *nominal voltage* of the *system* at the point of evaluation.

For non-three-phase *facilities*, the reference current corresponds to the current for a three-phase *facility* with the same power.

## 3.4 FACILITY OPERATING CONDITIONS

The *facility* operating conditions discussed below are also used as input for the detailed assessment of emission limit compliance.

Specific general or occasional operating conditions of the *facility* may be indicated by Hydro-Québec.

### 3.4.1 General facility operating conditions

The general operating conditions of the *facility* include the most unfavorable and frequent or prolonged operating conditions of the *facility* — typically following a single-element contingency (n-1) — the overall statistical likelihood of which is greater than 5% over one year.

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### 3.4.2 Occasional facility operating conditions

The occasional operating conditions of the *facility* include the operating conditions the overall statistical likelihood of which does not exceed 5% over one year. They correspond in particular to equipment outages under degraded conditions that may occur occasionally and result in higher emission levels.

## 3.5 EMISSION STUDY

An emission study is carried out, for each *disturbance*, to demonstrate that the maximum anticipated emission level of the *facility* does not exceed emission limits at the point of evaluation.

The emission study identifies and takes into account any corrective equipment and mitigation measures required to comply with emission limits.

The emission study must be performed by an engineer (whose title and practice are subject to the laws, codes and regulations applicable in Québec).

The emission study includes the required information and results for each *disturbance*.

The emission level is to be assessed using the methods including the *Transmission System* parameters and the *facility* operating conditions.

## 3.6 MEASUREMENT OF EMISSION LEVELS

Whenever Hydro-Québec requires a measurement report to be submitted, the measures in question must be made in accordance with a measurement protocol approved by Hydro-Québec.

The measurement protocol specifies in particular the methods for measurement and analysis of results, as well as any tests to be performed.

In light of measurements made by the *Transmission Provider*, Hydro-Québec may require a new assessment of compliance with emission limits, as well as the implementation of mitigation measures or operating restrictions for the *facility*, should the *facility* not comply with emission limits.

## 3.7 REQUIRED INFORMATION

The detailed assessment must at least contain the information indicated below:

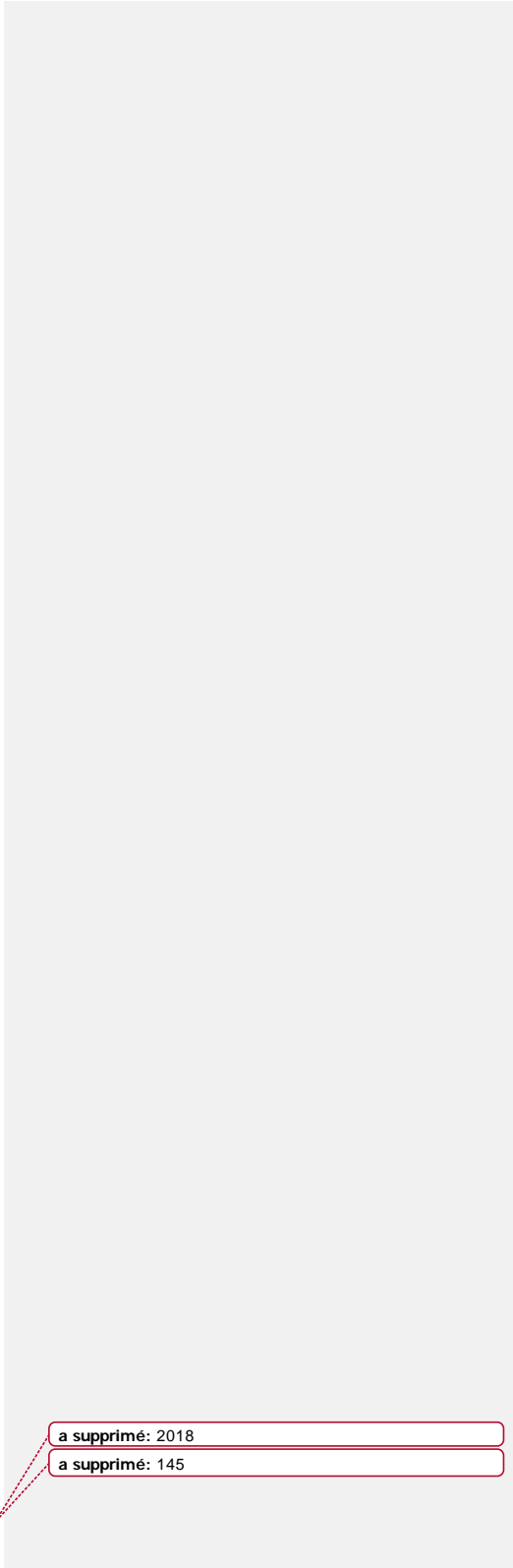
- Single-line diagram of the *facility* and key electrical characteristics of the main *facility* equipment
- Reference power ( $S_r$ ) of the *facility*
- *System* short-circuit power ( $S_{sc}$ ) under general [conditions](#) and [under](#) occasional conditions, as supplied by Hydro-Québec
- General electrical characteristics and operating modes of disturbing equipment (e.g., power and types of converters, pulse numbers, impedances, short-circuit power, power and types of motors, inrush current and load cycles)
- Statement and justification of any assumption made in the course of assessing maximum *disturbance* emission levels

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- General electrical characteristics of any corrective equipment (e.g., harmonic filters, motor starters, current-limiting series reactors and reactive power compensators)
- Description of general and occasional *facility* operating conditions taken into account



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## 4 RAPID VOLTAGE CHANGES (RVC)

Rapid voltage changes (RVC) are sudden random or cyclical variations in the RMS voltage between two successive voltage levels, [within the voltage range bounded by the voltage dip and temporary overvoltage thresholds defined in the document \*Caractéristiques de la tension fournie par le réseau de transport d'Hydro-Québec\*<sup>1</sup>](#). Transient non-repetitive *disturbances* lasting less than two 60-Hz cycles (or 33.3 ms) are generally ignored in the assessment of RVC levels.

RVCs are in particular caused by switching operations (e.g., capacitor banks) which produce rapid changes in reactive power, at the startup and the stop of power equipment (e.g., motors  $\geq 500$  hp), [at the startup or rapid power changes of generators or wind turbines, and at power transformer energization.](#)

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RVC emission limits apply to voltage changes that occur no more than 10 times per hour.

### 4.1 SIMPLIFIED ASSESSMENT

To be eligible for the simplified assessment:

- The *facility* must not include any equipment whose power demand or fluctuations may cause RVC, [including power transformers if the facility has a  \$S\_{sc, general}/S\_r\$  ratio of  \$< 20\$](#)
- A diagram of the *facility* showing all electric equipment (e.g., motors and furnaces) and a written confirmation that their operating mode will not cause any RVC must be submitted to Hydro-Québec.

### 4.2 RVC EMISSION LIMITS

Table 1: RVC emission limits

Repetition rate $f_{RVC}$ (changes/hour)	$\Delta U_{3s}/U$ (%)	$\Delta U_{3s}/U$ (%)
	Under general conditions	Under occasional conditions
$f_{VRT} \leq 2$	3	6
$2 < f_{VRT} \leq 10$	2.5	5

Note: A drop in voltage followed by a rise, or vice versa, counts as two voltage changes.

These limits are defined according to the number of RVCs that may occur in one hour ( $f_{RVC}$ ); they are expressed as the percent ratio of the RMS voltage change (averaged over 3 seconds) to the *Transmission System* voltage level ( $\Delta U_{3s}/U$ ).

These emission limits apply to each of the three phases; whichever emission level is the highest must comply with these limits.

Emission limits under general [conditions](#) and [under](#) occasional conditions apply to any *facility*, irrespectively of the  $S_{sc, general}/S_r$  ratio.

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<sup>1</sup> [Reference provided for explanatory and information purposes only.](#)

### 4.3 RVC EMISSION LEVELS

Maximum RVC emission levels must be assessed for each of the three phases.

Emission levels are evaluated under general [conditions](#) and [under](#) occasional [conditions](#).

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Emission levels under general conditions are the emission levels generated when the *Transmission System* operates under general conditions ( $S_{sc, general}$ ).

Emission levels under occasional conditions are the emission levels generated when the *Transmission System* operates under occasional conditions ( $S_{sc, occasional}$ ).

RVC emission levels may be approximated by the relative voltage change  $d$  ( $\Delta U/U_{nom}$ ). Guidance on how to calculate the relative voltage change is provided by standard CAN/CSA C61000-3-7<sup>2</sup> (paragraph E.1.2: *Simplified calculation of the relative voltage change d*).

Detailed parameters for calculating RVC levels are given in Appendix [B](#).

[For initial energization of the power transformer, assessing emission levels takes into account the main influencing parameters based on current industry best practices, e.g., initial conditions such as residual flux and the moment when the transformer is switched on, its magnetization curve and leak impedance, the system's short-circuit parameters and the sympathetic effect of other power transformers. Guidance on this assessment is provided by the CIGRE 568 brochure, "Transformer energization in power systems: A study guide."<sup>3</sup>](#)

### 4.4 RVC EMISSION STUDY

If Hydro-Québec requires a RVC emission study, it must be carried out under general [conditions](#) and [under](#) occasional conditions for all *facilities*, irrespectively of the  $S_{sc, general}/S_r$  ratio.

The RVC emission study must present the following results:

- For each piece or set of equipment: its characteristics, active and reactive power fluctuations ( $\Delta P$  and  $\Delta Q$ , respectively) and their repetition rate ( $f_{RVC}$ )
- Description of any mitigation measures, including planned restrictions on operating conditions, and their effect on emission levels
- [Table of RVC emission levels \( \$\Delta U\_{3s}/U\$ \) and their repetition rates \( \$f\_{RVC}\$ \), including any mitigation measures](#)
- [If  \$S\_{sc, general}/S\_r < 20\$ :](#)
  - [The maximum emission level for RVC caused by energizing the \*facility's\* power transformers](#)
  - [A graph showing the RMS voltage \(over 1/60 s\) for at least the first 3 seconds, the influencing parameters and the assumptions taken into account in the assessment](#)
  - [The characteristics of any required mitigation measures](#)

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<sup>2</sup> Reference provided for explanatory and informational purposes only.

<sup>3</sup> See note 2.

## 5 FLICKER

Flicker is the impression of unsteadiness of visual sensation induced by a light stimulus whose luminance or spectral distribution fluctuates over time. Flicker is the effect on lighting of repetitive voltage changes at frequencies to which the human eye is particularly sensitive, especially from 0.1 to 25 Hz.

These repetitive voltage changes can be attributed to equipment such as arc or induction furnaces, electric welding machines, generators or wind turbines producing rapid power changes, to variable-power process equipment (e.g., presses, winches, rolling mills), and to frequent motor startups.

Flicker refers to voltage changes that occur more than 10 times per hour.

### 5.1 SIMPLIFIED ASSESSMENT

To be eligible for the simplified assessment:

- Relative voltage changes ( $\Delta U/U_{nom}$ ) must be less than or equal to the limits indicated in Table 2, under general operating conditions (i.e., taking into account  $S_{sc, general}$  and the *facility* general operating conditions)

**Table 2: Emission limits for relative voltage changes ( $\Delta U/U_{nom}$ )**

Repetition rate $f_d$ (changes/minute)	$\Delta U/U_{nom}$ (%)
$0.17 < f_d \leq 0.5$	1.5
$0.5 < f_d \leq 1$	0.8
$1 < f_d \leq 10$	0.4
$10 < f_d \leq 200$	0.2
$200 < f_d$	0.1

Note: A drop in voltage followed by a rise, or vice versa, counts as two voltage changes.

These limits are defined according to the number of changes that may occur per minute ( $f_d$ ) of the voltage changes that may cause flicker; they are expressed as the percent ratio of the RMS voltage change (over 1/60 s) to the nominal *Transmission System* voltage ( $\Delta U/U_{nom}$ ). Guidance on how to calculate the relative voltage change  $\Delta U/U_{nom}$  is provided by standard CAN/CSA C61000 3 7<sup>4</sup> (paragraph E.1.2: *Simplified calculation of the relative voltage change d*).

If several pieces or sets of equipment produce voltage changes ( $\Delta U$ ) simultaneously at repetition rates ( $f_d$ ) indicated in Table 2, the relative voltage change ( $\Delta U/U_{nom}$ ) limit for each piece or set of equipment must then be divided by  $\sqrt[3]{X}$ , where  $X$  is the total number of pieces or sets of equipment involved.

- Written confirmation must be submitted to Hydro-Québec, including the results indicated below:
  - For each piece or set of equipment: its characteristics, its active and reactive power fluctuations ( $\Delta P$  and  $\Delta Q$ , respectively) and their repetition rate ( $f_d$ )

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- Table of calculated relative voltage changes ( $\Delta U/U_{nom}$ ) and their respective repetition rates ( $f_d$ )

## 5.2 EMISSION LIMITS FOR FLICKER

**Table 3: Emission limits for flicker ( $P_{st}$ )**

Under	Limits for severity index $P_{st}$ (short-term flicker)
General conditions	0.3
Occasional conditions	0.45

If any emission limit is exceeded, the *Transmission Providers* shall determine whether it may be raised based on the characteristics of the *system* under study and guidance provided by standard CAN/CSA-C61000-3-7<sup>5</sup>.

These emission limits apply to each of the three phases; whichever emission level is the highest must comply with these limits.

Emission limits under general [conditions](#) and [under](#) occasional conditions apply to any *facility*, irrespectively of the  $S_{sc, general}/S_r$  ratio.

## 5.3 EMISSION LEVELS FOR FLICKER

Maximum flicker emission levels must be assessed for each of the three phases.

Emission levels are evaluated under general [conditions](#) and [under](#) occasional conditions.

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Emission levels under general conditions are the emission levels generated when both the *facility* and the *Transmission System* ( $S_{sc, general}$ ) operate under general conditions.

Emission levels under occasional conditions are the emission levels generated when the *facility* or the *Transmission System* ( $S_{sc, occasional}$ ) operate under occasional conditions.

Guidance on how to assess emission levels for flicker ( $P_{st}$ ), including summation methods used to calculate the combined effect of flicker causing equipment, is provided in Appendix E of standard CAN/CSA-C61000-3-7<sup>6</sup>.

## 5.4 EMISSION STUDY FOR FLICKER

If Hydro-Québec requires the emission study for flicker, it must be carried out:

- under general conditions, if  $S_{sc, general}/S_r \geq 30$
- under general [conditions](#) and [under](#) occasional conditions, if  $S_{sc, general}/S_r < 30$

The emission study for flicker must present the results indicated below:

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5 Reference provided for explanatory and information purposes [only](#).

6 See note 3.



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- Description of the electrical and operational characteristics of disturbing equipment, e.g.:
  - for arc furnaces: impedance and short-circuit power levels, type of process, type of raw material used in the furnace, operating cycles
  - for motors: power and type of motors, inrush currents, frequency of startups and load cycles
- For each piece or set of equipment: its characteristics, its active and reactive power fluctuations ( $\Delta P$  and  $\Delta Q$ , respectively) and their repetition rate ( $f_d$ )
- Table of calculated relative voltage changes ( $\Delta U/U_{nom}$ ) and their respective repetition rates ( $f_d$ )
- Summation methods used to calculate the combined effect of flicker causing equipment, including a justification for their use based on equipment operating modes
- Resulting emission level for flicker ( $P_{st}$ ) at the point of evaluation and applicable emission limit

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## 6 LOAD OR CURRENT UNBALANCE

Load or current unbalance results from the design or operation of a *facility* or piece of equipment (e.g., arc or induction furnaces, single- or two-phase loads or generators, and electric train alternating current power supply systems) whose current (or power consumption or generation) unbalance may cause a voltage unbalance on the *system*.

A current (or voltage) unbalance arises when the three currents (or voltages) of a three-phase *system* are not of equal magnitude or are not phase-shifted 120 degrees from one another.

The unbalance considered herein involves the negative-sequence component of 60-Hz currents or voltages calculated using the symmetrical component method (Fortescue’s transformation).

### 6.1 SIMPLIFIED ASSESSMENT

To be eligible for the simplified assessment:

- $I_2/I_{sc}$  (or  $S_{single-phase}/S_{sc, general}$ )  $< 0.2\%$ , where:
  - $I_2$  = Negative-sequence component of the *facility* current
  - $I_{sc}$  = Three-phase short-circuit current of the system, calculated using  $S_{sc, general}$
  - $S_{single-phase}$  = Single-phase load (or power) equivalent to the imbalance of the *facility*
- Written confirmation of the value of the single-phase power equivalent ( $S_{single-phase}$ ) to the *facility*’s load or current unbalance must be submitted to Hydro-Québec.

### 6.2 EMISSION LIMITS FOR LOAD OR CURRENT UNBALANCE

ply to all *facilities*, except those that include electric train power supply systems, to which emission limits for voltage load unbalance apply.

Emission limits under general [conditions](#) and [under](#) occasional conditions apply to any *facility*, irrespectively of the  $S_{sc, general}/S_r$  ratio.

#### 6.2.1 Emission limits for current unbalance — facilities

Table 4: Limits for negative-sequence component ratio ( $I_2 / I_r$ )

$S_{sc, general}/S_r$	$I_2/I_r$ (%)	$I_2/I_r$ (%)
	Under general conditions	Under occasional conditions
5	4	6
20	7	10.5
50	13	19.5
100	20	30
200	30	45

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These limits apply to the current unbalance ratio ( $I_2/I_r$ ) expressed as a percent, where:

- $I_2$  = Negative-sequence component of the current due to the power unbalance of the *facility* ( $A_{rms}$ )
- $I_r$  = Reference current for the *facility* ( $A_{rms}$ ).

Emission limits applicable to any given *facility* depend on its  $S_{sc, general}/S_r$  ratio; they are calculated as follows:

- a) If  $5 \leq S_{sc, general}/S_r < 200$ , the emission limit is calculated according to Equation 1, i.e. using a linear interpolation between two consecutive limits specified in Table 4.

$$\text{Limit applicable to the facility} = \left[ \frac{(\text{LIMIT})_B - (\text{LIMIT})_A}{\left(\frac{S_{sc}}{S_r}\right)_B - \left(\frac{S_{sc}}{S_r}\right)_A} \right] \cdot \left[ \left(\frac{S_{sc}}{S_r}\right)_f - \left(\frac{S_{sc}}{S_r}\right)_A \right] + (\text{LIMIT})_A \quad (1)$$

Where:

- $f$  = Refers to the *facility* under study
- $A$  = Refers to the row in Table 4 containing the highest  $S_{sc, general}/S_r$  ratio that is less than the value for the *facility*
- $B$  = Refers to the row in Table 4 containing the lowest  $S_{sc, general}/S_r$  ratio that is greater than the value for the *facility*
- LIMIT = Limit found in Table 4.
- $S_{sc} = S_{sc, general}$

- b) If  $S_{sc, general}/S_r \geq 200$ , the percent emission limit under general conditions equals 30% and the limit under occasional conditions equals 45%.
- c) If  $S_{sc, general}/S_r < 5$ , the *Transmission Provider* determines the specific emission limit and conditions applicable to the *facility* under study, based on the characteristics of the system under study and guidance provided by standard CAN/CSA-C61000-3-13<sup>7</sup>.

### 6.2.2 Emission limits for voltage unbalance — electric trains

Table 5: Emission limits for voltage unbalance ( $U_2/U_1$ )

Under	$U_2/U_1$ (%)
General conditions	0.2
Occasional conditions	0.3

This emission limit applies to the negative-sequence voltage unbalance, expressed at the percent ratio of the negative-sequence voltage to the positive-sequence voltage ( $U_2/U_1$ ) for the *facility* under study.

If any limit is exceeded, the *Transmission Provider* shall determine whether it may be raised based on the characteristics of the system under study and guidance provided by standard CAN/CSA C61000-3-13<sup>8</sup>.

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### 6.3 EMISSION LEVELS FOR LOAD OR CURRENT UNBALANCE

Maximum emission levels must be assessed for load or current unbalance.

Emission levels are evaluated under general [conditions](#) and [under](#) occasional conditions.

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Emission levels under general conditions are the emission levels generated when both the *facility* and the *Transmission System* ( $S_{sc, general}$ ) operate under general conditions.

Emission levels under occasional conditions are the emission levels generated when the *facility* or the *Transmission System* ( $S_{sc, occasional}$ ) operate under occasional conditions.

An unbalanced three-phase *system* is assessed using the symmetrical component method (Fortescue's transformation). In general, it consists in calculating the negative-sequence component of the line current ( $I_2$ ) at the point of evaluation.

For complex cases, assessing unbalance emission levels requires the use of appropriate computer tools and models.

Anticipated emission levels of the *facility* do not include negative-sequence currents arising from *Transmission System* voltage unbalance that are not due to unbalanced *facility* power conditions.

### 6.4 EMISSION STUDY FOR LOAD OR CURRENT UNBALANCE

If Hydro-Québec requires the emission study for load or current unbalance, it must be carried out:

- Under general conditions, if  $S_{sc, general}/S_r \geq 30$
- Under general [conditions](#) and [under](#) occasional conditions, if  $S_{sc, general}/S_r < 30$

The emission study for load or current unbalance must present the results indicated below:

- List of power levels for equipment that produces load or current unbalance, their operating and connection modes
- Description of any mitigation measures
- Table of maximum emission levels for current unbalance (negative-sequence component) for the various operating modes

If required, Hydro-Québec may specify the phases onto which the unbalanced power must be redistributed so as to reduce the resulting level of voltage unbalance on the Transmission System.

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## 7 HARMONICS

Harmonics are sinusoidal voltages or currents having frequencies that are integral multiples of the fundamental frequency of the system (60 Hz).

Emission limits for harmonics include emission limits for harmonic currents and emission limits for telephone influence [and the harmonic amplification limit](#).

Harmonics are mainly caused by harmonics-producing equipment (e.g., arc or induction furnaces, rectifiers used for electrolysis, motor drives, frequency converters, and alternating current load controllers). Harmonics can also be amplified, [for example, by capacitor banks, cables and a low resistive load](#).

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### 7.1 SIMPLIFIED ASSESSMENT

To be eligible for the simplified assessment:

- The total three-phase power of harmonics-producing equipment<sup>9</sup> used at the *facility* must be:
  - less than or equal to the power indicated in Table 6

Table 6: Maximum total three-phase power

Voltage level (kV)	Maximum total three-phase power of harmonics-producing equipment (MVA)
44, 49	1
69	1.5
120	2.7
161	3.6
230	5
315, 345	7

- less than 0.25% of the short-circuit power under general *Transmission System* operating conditions ( $S_{sc, general}$ )
- Written confirmation of the total three-phase power of harmonics-producing equipment must be submitted to Hydro-Québec.

### 7.2 EMISSION LIMITS FOR HARMONICS

[The emission limits for harmonics include emissions limits for harmonic currents and the harmonic amplification factor limit](#).

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<sup>9</sup> Harmonics-producing equipment do not include *synchronous or asynchronous generators* if, regarding harmonics and telephone interference, they comply with IEC (International Electrotechnical Commission) 60034-series standards or ANSI (American National Standards Institute) C50-series standards. These references are provided [for explanatory and information purposes only](#).

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### 7.2.1 Emission limits for harmonic currents

Emission limits apply to each of the three phases. The highest emission level of individual harmonic currents ( $I_{h,n}/I_r$ ) for each harmonic order  $n = 2$  to 50, as well as the total harmonic distortion in current (THD<sub>I</sub>), must [comply with](#) those limits.

Emission limits under general [conditions](#) and [under](#) occasional conditions apply to any *facility*, irrespectively of the  $S_{sc, general}/S_r$  ratio.

Tables and present limits applicable, respectively, to odd and even percent ratios of individual harmonic currents ( $I_{h,n}/I_r$ ) under general conditions, where:

- $I_{h,n}$  = Harmonic currents of order  $n = 2$  to 50 ( $A_{rms}$ )
- $I_r$  = Reference current for the *facility* ( $A_{rms}$ )

**Table 7: Limits for individual odd harmonic current ratios ( $I_{h,n}/I_r$ ) (%),**

$S_{sc, general}/S_r$	n=3	n=5	n=7	n=9	n=11, 13	15≤n<23	23≤n<35	35≤n<50
5	1	1.2	0.8	0.5	0.5	0.4	0.3	0.2
20	1.5	2	1.5	0.75	1	0.65	0.45	0.3
50	2	3	2	1	1.5	1	0.7	0.5
200	4	6	4	2	3	2	1	0.7

Note: Under occasional conditions, emission limits for individual odd harmonic current ratios correspond to 1.5 times these emission limits

**Table 8: Limits for individual even harmonic current ratios ( $I_{h,n}/I_r$ ) (%),**

$S_{sc, general}/S_r$	n=2	n=4	n=6	n=8	10≤n≤50
5	0.75	0.5	0.3	0.2	0.15
20	1.1	0.75	0.45	0.3	0.25
50	1.5	1	0.6	0.4	0.3
200	2.2	1.5	1	0.6	0.4

Note: Under occasional conditions, emission limits for individual even harmonic current ratios correspond to 1.5 times these emission limits.

Table 9 presents limits applicable to the total harmonic distortion in current (THD<sub>I</sub>), as defined by Equation 2.

$$THD_I = \frac{1}{I_r} \sqrt{\sum_{n=2}^{50} I_{h,n}^2} \times 100\% \quad (2)$$

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**Table 9: Limits for the total harmonic distortion in current (THD<sub>i</sub>), under general conditions**

$S_{sc, general}/S_r$	THD <sub>i</sub> (%)
5	1.7
20	3
50	4.5
200	6

Note: Under occasional conditions, emission limits for the total harmonic distortion in current correspond to 1.5 times these emission limits

Emission limits applicable to any given *facility* depend on its  $S_{sc, general}/S_r$  ratio; they are calculated as follows:

- a) If  $5 \leq S_{sc, general}/S_r < 200$ , the emission limit is calculated according to Equation 3, i.e. using a linear interpolation between two consecutive limits specified in tables, and 9.

Limit applicable to the *facility*

$$= \left[ \frac{(LIMIT)_B - (LIMIT)_A}{\left(\frac{S_{sc}}{S_r}\right)_B - \left(\frac{S_{sc}}{S_r}\right)_A} \right] \cdot \left[ \left(\frac{S_{sc}}{S_r}\right)_f - \left(\frac{S_{sc}}{S_r}\right)_A \right] + (LIMIT)_A \quad (3)$$

Where:

- f = Refers to the *facility* under study
- A = Refers to the row in tables, or 9 containing the highest  $S_{sc, general}/S_r$  ratio that is less than the value for the *facility*
- B = Refers to the row in tables, or 9 containing the lowest  $S_{sc, general}/S_r$  ratio that is greater than the value for the *facility*
- LIMIT = Limit found in tables, or 9
- $S_{sc} = S_{sc, general}$

- b) If  $S_{sc, general}/S_r \geq 200$ , the emission limit is calculated according to Equation 4, i.e. the limit is proportional to the  $S_{sc, general}/S_r$  ratio of the *facility*

Limite applicable to the *facility*

$$= \left[ \left(\frac{S_{sc}}{S_r}\right)_f \div 200 \right] \cdot (LIMIT)_{200} \quad (4)$$

- c) If  $S_{sc, general}/S_r < 5$ , the *Transmission Provider* determines the specific emission limit and conditions applicable to the *facility* under study based on the characteristics of the *system* under study and guidance provided by standard CAN/CSA-C61000-3-6<sup>10</sup>.

### 7.2.2 Harmonic amplification factor limit

[A limit applies to the amplification of the pre-existing harmonic voltage in the \*Transmission System\* at the point of evaluation.](#)

<sup>10</sup> Reference provided for explanatory and information purposes only.

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The highest harmonic amplification factor ( $FA_n$ ) for each harmonic of orders  $n = 2$  to  $50$  must comply with the limit.

The harmonic amplification factor limit applies under general conditions and under occasional conditions to any facilities, irrespectively of the  $S_{sc\_general}/S_r$  ratio.

Table 10 presents limits applicable to the harmonic amplification factor ( $FA_n$ ), defined according to Equation 5.

$$FA_n = \frac{Z_{n, facility}}{Z_{n, facility} + Z_{n, system}} \quad (5)$$

Where:

$Z_{n, facility}$  = Complex impedance (in ohm) of the facility at harmonic order  $n$  as seen from the Transmission System connection point

$Z_{n, system}$  = Complex impedance (in ohm) of the harmonic impedance locus of the system (see 7.4.1) at harmonic order  $n$ , which maximizes the amplification factor ( $FA_n$ )

**Table 10: Harmonic amplification factor limit ( $FA_n$ ) under general conditions and under occasional conditions**

Harmonic order $n$	$FA_n$
$2 \leq n \leq 50$	1.5

If any limit is exceeded, the Transmission Provider determines whether it may be raised based on the characteristics of the system under study and the involved harmonic order  $n$ .

### 7.3 EMISSION LIMITS FOR TELEPHONE INFLUENCE

The emission limit for telephone influence is applicable to the  $I \cdot T_{balanced}$  product, defined by Equation 6.

$$I \cdot T_{balanced} = \sqrt{\sum_{n=2}^{50} (I_{h,n} \cdot W_n)^2} \quad (A \text{ weighted}) \quad (6)$$

Where:

$I_{h,n}$  = Harmonic currents of order  $n = 2$  to  $50$  ( $A_{rms}$ )

$W_n$  = Weighting factor given in Table 11

**Table 11: Weighting factors  $W_n$  for telephone influence**

$n$	F(Hz)	$W_n$	$n$	F(Hz)	$W_n$
-	-	-	26	1 560	6 790
2	120	10	27	1 620	6 970
3	180	30	28	1 680	7 060
4	240	105	29	1 740	7 320
5	300	225	30	1 800	7 570

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n	F(Hz)	W <sub>n</sub>	n	F(Hz)	W <sub>n</sub>
6	360	400	31	1 860	7 820
7	420	650	32	1 920	8 070
8	480	950	33	1 980	8 330
9	540	1 320	34	2 040	8 580
10	600	1 790	35	2 100	8 830
11	660	2 260	36	2 160	9 080
12	720	2 760	37	2 220	9 330
13	780	3 360	38	2 280	9 590
14	840	3 830	39	2 340	9 840
15	900	4 350	40	2 400	10 090
16	960	4 690	41	2 460	10 340
17	1 020	5 100	42	2 520	10 480
18	1 080	5 400	43	2 580	10 600
19	1 140	5 630	44	2 640	10 610
20	1 200	5 860	45	2 700	10 480
21	1 260	6 050	46	2 760	10 350
22	1 320	6 230	47	2 820	10 210
23	1 380	6 370	48	2 880	9 960
24	1 440	6 650	49	2 940	9 820
25	1 500	6 680	50	3 000	9 670

**Table 12: Emission limits for telephone influence (I·T<sub>balanced</sub> product)**

Under	Limit for I·T <sub>balanced</sub> product (A <sub>weighted</sub> )
General conditions	20,000
Occasional conditions	30,000

These emission limits apply to each of the three phases; whichever emission level is the highest must comply with these limits.

Emission limits under general [conditions](#) and [under](#) occasional conditions apply to any *facility*, irrespectively of the S<sub>sc</sub> general/S<sub>r</sub> ratio.

### 7.3.1 Specific limit

If the I·T<sub>balanced</sub> product exceeds the applicable limit indicated in [Table 12](#), the *Transmission Provider* may allow the use of a higher specific limit depending on any one of the factors indicated below (the detailed calculation of which must be submitted to Hydro-Québec):

- Distance separating the power lines affected and telephone lines

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- Equivalent soil resistivity along the power lines affected
- Total equivalent length over which individual telephone lines run parallel to power lines affected

The *Transmission Provider* also determines which specific conditions apply and must receive drawings showing the relative geographic location of telephone lines near (<10 km) affected power lines.

If the  $I \cdot T_{\text{balanced}}$  product exceeds the applicable limit indicated in [Table 12](#), the *Transmission Provider* shall indicate which transmission lines are affected upon request.

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### 7.3.2 Exemption

The *Transmission Provider* may grant an exemption if it receives a document certifying that there is no existing or planned voice-frequency analog telephone line within 10 km of the transmission lines affected.

If the  $I \cdot T_{\text{balanced}}$  product exceeds the applicable limit indicated in [Table 12](#), the *Transmission Provider* shall indicate which transmission lines are affected upon request.

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## 7.4 EMISSION LEVELS FOR HARMONICS

[The emission level for harmonics refers to the emission levels for the facility's harmonic currents and the harmonic amplification of the Transmission System's pre-existing voltage caused by the facility interacting with the system.](#)

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Maximum emission levels for each individual odd and even harmonic current ( $I_{h,n}/I_r$ ), as well as the total harmonic distortion in current (THD<sub>I</sub>), must be evaluated for each of the three phases, taking into account all harmonics of orders  $n = 2$  to 50. A harmonic current is a harmonic line current circulating at the point of evaluation.

[The maximum harmonic amplification factor \(FA<sub>n</sub>\) must be evaluated for all harmonics of orders  \$n = 2\$  to 50.](#)

Emission levels are evaluated under general [conditions](#) and [under occasional conditions](#).

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Emission levels under general conditions are the emission levels generated when the *facility* operates under general conditions.

Emission levels under occasional conditions are the emission levels generated when the *facility* operates under occasional conditions.

Emission levels are evaluated taking into account harmonic impedance loci, non-characteristic harmonic emissions [as well as](#) fluctuating harmonics [and interharmonics](#), which are presented in sections 7.4.1, 7.4.2 and 7.4.3, respectively.

Guidance on how to assess emission levels for harmonic currents is provided in section 6.3 of standard CAN/CSA-C61000-3-6<sup>11</sup>.

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<sup>11</sup> Reference provided only for explanatory and informative purposes.

In addition to these guidelines, the document *Caractéristiques de la tension fournie par le réseau de transport d'Hydro-Québec*<sup>12</sup> provides information on *disturbance* levels that may be found on the Hydro-Québec *Transmission System*.

When assessing the *facility's* emission levels for harmonic currents, harmonic filter performance must take into account the variation of  $\pm 0.2$  Hz of the frequency on the *Transmission System*. Asymmetries generated by the *facility's* equipment must be added to that.

#### 7.4.1 Harmonic impedance loci

The *Transmission Provider* shall provide information on harmonic impedance loci of the *system* upon request.

This data corresponds to the parameters defining a range of possible impedances seen looking into the *system* from the point of evaluation, for harmonic orders  $n = 2$  to 50.

Harmonic impedance loci serve as input to assess harmonic emission levels for a given *facility*, including the harmonic amplification factor ( $FA_n$ ).

*System* harmonic impedance loci do not include the effect of the *facility* under study. That effect must be taken into account in assessing the emission levels. The interaction between the *facility* and the *system*, for example the interaction between *facility* capacitors or filters and the *system*, can create resonances, which could amplify harmonic levels on the *Transmission System*. The harmonic amplification factors ( $FA_n$ ) must stay within the limit. Emission levels for harmonic currents must take into account potential resonances and fall below emission limits.

After having assessed all sources of harmonics of orders  $n = 2$  to 50 among equipment used in the *facility* under study (including any non-characteristic or fluctuating harmonics and interharmonics), maximum emission levels for individual harmonic currents ( $I_{h,n}/I_r$ ) and total harmonic distortion in current (THD<sub>i</sub>) must be evaluated by selecting the combinations of *system* impedance (impedance loci) and *facility* impedance (different operating conditions of the *facility*) that maximize emission levels. This may require successive iterations or an appropriate optimization algorithm.

The harmonic amplification factors ( $FA_n$ ) must be evaluated by determining the combinations of the *system's* impedance (impedance loci) and the *facility's* impedance (different *facility* operating conditions) that maximize amplification, irrespectively of the resulting emission levels for harmonic currents.

#### 7.4.2 Emission of non-characteristic harmonics

So-called "non-characteristic" harmonics are generated by a *facility* due to the existence of some degree of dissymmetry within the *Transmission System* and the *facility* in question.

Guidance for assessing sources of non-characteristic harmonics within a given *facility* is provided in section 6.3.2 of standard CAN/CSA-C61000-3-6<sup>13</sup>.

<sup>12</sup> See note 9.

<sup>13</sup> See note 9.

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In addition to these guidelines, [Table 13](#) specifies the voltage unbalance ratio, which reflects the degree of dissymmetry to be taken into account on the *Transmission System* when assessing emission levels for non-characteristic harmonics. Asymmetries generated by the *facility's* equipment must be added to that.

**Table 13: *Transmission System* voltage unbalance ratios ( $U_2/U_1$ ) specified according to *nominal voltage* at the point of evaluation, for the evaluation of emission levels of non-characteristic harmonics**

Nominal voltage of the system	$U_2/U_1$
230 kV, 315 kV and 345 kV	1.5%
69 kV, 120 kV and 161 kV	2%
44 kV and 49 kV	2%

### 7.4.3 Fluctuating harmonics and interharmonics

If harmonics are continuously and rapidly fluctuating, the evaluation of emission levels for harmonic currents relies on the harmonic group and subgroup method as explained in standard CAN/CSA-IEC 61000-4-7<sup>14</sup>. Examples are given in Appendix C.3 *Fluctuating harmonics* of this standard.

[When the facility emits interharmonics \(see chapter 8\), the emission level for harmonic currents is evaluated by the RMS value of the harmonic group as defined in standard CAN/CSA-IEC 61000-4-7 \[1\].](#)

## 7.5 EMISSION LEVELS FOR TELEPHONE INFLUENCE

Emission levels for telephone influence ( $I \cdot T_{\text{balanced}}$  product) are calculated using Equation 6 based on the above-defined emission levels for harmonic currents of orders  $n = 2$  to 50.

Maximum emission levels must be evaluated for each of the three phases.

The  $I \cdot T_{\text{balanced}}$  product may be calculated taking into account the potential simultaneity of emission levels for all harmonics for different general or occasional *facility* operating conditions and different *system* harmonic impedance values (impedance loci). The highest emission level obtained must [comply with](#) the telephone influence limit.

## 7.6 EMISSION STUDY FOR HARMONICS

If Hydro-Québec requires the emission study for harmonics, it must be carried out:

- under general conditions, if  $S_{sc, \text{general}}/S_r \geq 30$
- under general [conditions](#) and [under](#) occasional conditions, if  $S_{sc, \text{general}}/S_r < 30$

<sup>14</sup> In this document, a number in square brackets refers to the document numbered in the list of mandatory reference documents.

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The emission study for harmonics must present emission levels that take into account:

- harmonic impedance loci, as supplied by Hydro-Québec, if  $S_{sc, general}/S_r < 100$
- non-characteristic harmonic emissions, if  $S_{sc, general}/S_r < 30$
- any fluctuating harmonics [and interharmonics](#)

The emission study for harmonics must present the following results:

- Relevant facility specifications, particularly regarding the characteristics of capacitor banks and filters, as well as assumptions regarding filter detuning and the angular displacement between converter units
- Data for harmonic converter models (using the Thévenin/Norton circuit), where appropriate, and for circuit characteristics (e.g., filters) modeling each source, for harmonics of the orders  $n = 2$  to 50 and all operating conditions
- Potential resonances for example between the *facility's* capacitors, filters or cables and the *system*
- Tables of results, for harmonics of orders  $n = 2$  to 50, under general conditions and, if required, under occasional conditions, presenting:
  - Maximum harmonic amplification factor ( $FA_n$ ) for each order
  - System harmonic impedance values that maximize each harmonic amplification factor determined from the system's harmonic impedance loci, if applicable
    - Maximum harmonic currents generated by disturbing equipment within the *facility* under study, along with the respective angular displacements in the case of high pulse number converters represented by multiple equivalent harmonic current sources
    - *Facility* harmonic impedance values (amplitudes and angles), including capacitors and filters and the effect of detuning, possible switching operations, etc.
    - *System* harmonic impedance values that maximize each emission level for harmonic currents, based on system harmonic impedance loci, if applicable
    - Maximum emission levels for individual harmonic currents ( $I_{h,n}/I_r$ ), for each harmonic order
    - Maximum emission level for the total harmonic distortion in current (THDi) under the various operating conditions of the *facility*
- For emission levels for telephone influence under general conditions and, if required, occasional conditions:
  - Table of  $I \cdot T_{balanced}$  product calculations, for each harmonic order, under the various *facility* operating conditions
  - If the *Transmission Provider* has set any specific limit, drawings showing the relative geographic location of telephone lines and affected power lines, as well as detailed calculations of requested factors
  - If an exemption from emission limits for telephone influence is sought, a document certifying that there is no existing or planned voice-frequency analog telephone line within 10 km of the transmission lines affected

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## 8 INTERHARMONICS

Interharmonics are sinusoidal voltages or currents having frequencies between two consecutive harmonic frequencies. Interharmonic frequencies are not integral multiples of the fundamental frequency of the system (60 Hz).

Emission limits for interharmonics include emission limits for interharmonic currents and the harmonic (or interharmonic) amplification limit.

Interharmonics are mainly caused by interharmonics-producing equipment, for example: equipment using Voltage Source Converters (VSC), such as turbines or solar panels; frequency converters; and arc furnaces. Interharmonics can also be amplified, for example, by capacitor banks, cables and a low resistive load.

### 8.1 SIMPLIFIED ASSESSMENT

To be eligible for the simplified assessment:

- The total three-phase power of interharmonics-producing equipment used at the facility must be less than 2% of the short-circuit power under the Transmission System's general operating conditions ( $S_{sc,general}$ )
- Written confirmation of the total three-phase power of interharmonics-producing equipment must be submitted to Hydro-Québec

### 8.2 EMISSION LIMITS FOR INTERHARMONICS

Emission limits for interharmonics include emission limits for interharmonic currents and the interharmonic amplification factor limit.

#### 8.2.1 Emission limits for interharmonic currents

Emission limits apply to each of the three phases. The highest emission level of individual interharmonic currents ( $I_{ih,n}/I_r$ ) for each harmonic of orders  $n = 1$  to 49 must comply with those limits<sup>15</sup>.

Emission limits under general conditions and under occasional conditions apply to all facilities, irrespective of the  $S_{sc,general}/S_r$  ratio.

Table 14 presents limits applicable to percent ratios of individual interharmonic current ( $I_{ih,n}/I_r$ ) under general conditions, where:

<sup>15</sup> The numbering of interharmonic orders complies with standard CAN/CSA-IEC 61000-4-7 [1]. For example, the interharmonic centered subgroup with an average frequency of 150 Hz corresponds to interharmonic order 2 and so on.

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$I_{ih,n}$  = Interharmonic currents of interharmonic orders  $n = 1$  to 49 ( $A_{rms}$ ).  
 $I_r$  = Facility reference current ( $A_{rms}$ ).

**Table 14: Limits for individual interharmonic currents  $I_{ih,n}/I_r$  (%) under general conditions**

$S_{sc, general}/S_r$	$1 \leq n \leq 6$	$7 \leq n \leq 8$	$9 \leq n \leq 49$
5	0.3	0.2	0.15
20	0.45	0.3	0.25
50	0.6	0.4	0.3
200	1.0	0.6	0.4

Note: Under occasional conditions, emission limits for individual interharmonic current ratios correspond to 1.5 times these emission limits

Emission limits applicable to any given facility depend on its  $S_{sc, general}/S_r$  ratio; they are calculated as follows:

a) If  $5 \leq S_{sc, general}/S_r < 200$ , the emission limit is calculated according to Equation 7, i.e., using a linear interpolation between two consecutive limits specified in Table 14.

$$\frac{\text{Limit applicable to the facility}}{\text{the facility}} = \left[ \frac{(\text{LIMIT})_B - (\text{LIMIT})_A}{\left(\frac{S_{cc}}{S_r}\right)_B - \left(\frac{S_{cc}}{S_r}\right)_A} \right] \cdot \left[ \left(\frac{S_{cc}}{S_r}\right)_f - \left(\frac{S_{cc}}{S_r}\right)_A \right] + (\text{LIMIT})_A \quad (5)$$

Where:

- $f$  = Refers to the facility under study
- $A$  = Refers to the row in Table 14 containing the  $S_{sc, general}/S_r$  ratio that is less than the value for the facility
- $B$  = Refers to the row in Table 14 containing the  $S_{sc, general}/S_r$  ratio that is greater than the value for the facility
- LIMIT = Limit found in Table 14
- $S_{cc} = S_{sc, general}$

b) If  $S_{sc, general}/S_r \geq 200$ , the emission limit is calculated according to Equation 8, i.e., the limit is proportional to the  $S_{sc, general}/S_r$  ratio of the facility.

$$\frac{\text{Limit applicable to the facility}}{\text{the facility}} = \left[ \left(\frac{S_{cc}}{S_r}\right)_f \div 200 \right] \cdot (\text{LIMIT})_{200} \quad (8)$$

c) If  $S_{sc, general}/S_r < 5$ , the Transmission Provider determines the specific emission limit and conditions applicable to the facility under study based on the characteristics of the system under study and guidance provided by standard CAN/CSA C61000-3-6<sup>16</sup>.

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<sup>16</sup> Reference provided for explanatory and information purposes only.

### 8.2.2 Harmonic (or interharmonic) amplification factor limit

A limit applies to the amplification of the pre-existing harmonic (or interharmonic) voltage level in the Transmission System at the point of evaluation.

The harmonic amplification limit of orders  $n = 2$  to 50, as defined in Table 10 in section 7.2.2, is generally sufficient to limit interharmonic amplification of frequencies between 90 Hz and 2,990 Hz. This limit indeed applies to the harmonic group defined in standard CAN/CSA-IEC 61000-4-7 [1], grouping the harmonic with the interharmonics within the harmonic frequency range of  $\pm 30$  Hz.

For interharmonics with a frequency between 70 Hz and 90 Hz, the limit of **1.0** applies to the amplification factor of the interharmonic subgroup comprised of frequencies between 70 to 90 Hz ( $FA_{1+}$ ).

The highest amplification factor ( $FA_{1+}$ ) must comply with the limit.

The interharmonic amplification limit applies under general conditions and under occasional conditions at all facilities, independently of  $S_{sc\_general}/S_p$ .

The interharmonic amplification factor ( $FA_{1+}$ ) is defined according to Equation 9.

$$FA_{1+} = \frac{Z_{90Hz, facility}}{Z_{90Hz, facility} + Z_{90Hz, system}} \quad (9)$$

Where:

$Z_{90Hz, facility}$  = Complex impedance (in ohm) of the facility at the frequency of 90 Hz as seen from the Transmission System connection.

$Z_{90Hz, system}$  = Complex impedance (in ohm) calculated from the system short-circuit power (see section 3.3.2) and proportionally adjusted to the frequency of 90 Hz.

### 8.3 EMISSION LEVEL FOR INTERHARMONICS

The interharmonic emission level refers to the emission level for the facility's interharmonic currents and the interharmonic amplification of the Transmission System's pre-existing voltage caused by the facility interacting with the system.

An interharmonic is evaluated by the RMS value of the interharmonic centred subgroup as defined in the standard CAN/CSA-IEC 61000-4-7 [1].

The maximum emission level for each individual interharmonic current ( $I_{ih,n}/I_r$ ) must be evaluated for each of the three phases, taking into account all interharmonics of interharmonic orders  $n = 1$  to 49. An interharmonic current is an interharmonic line current circulating at the point of evaluation.

The evaluation of the interharmonic amplification factor for frequencies between 90 Hz and 2,990 Hz is not necessary due to the evaluation of the maximum harmonic amplification factor for harmonics of orders  $n = 2$  to 50 provided in section 7.4. Indeed, the harmonic group defined in standard CAN/CSA IEC 61000-4-7 [1] groups the harmonic with the interharmonics within the harmonic frequency range of  $\pm 30$  Hz.

For frequencies between 70 Hz and 90 Hz, the maximum interharmonic amplification factor ( $FA_{1+}$ ) must be evaluated according to Equation 9 in section 8.2.2.

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The emission level is evaluated under general conditions and under occasional conditions.

The emission level under general conditions are the emission levels generated when the facility operates under general conditions.

The emission level under occasional conditions are the emission levels when the facility operates under occasional conditions.

The emission level is evaluated taking into account the system's harmonic impedance loci described in section 7.4.1. In addition, each of the system's harmonic impedance loci includes a larger frequency range so that the harmonic group and interharmonic centred subgroup can be evaluated. The Transmission Provider provides a method of using the impedance locus to that effect.

Guidance on how to assess emission levels for harmonic and interharmonic currents is provided in section 6.3 of standard CAN/CSA C61000-3-6<sup>17</sup>.

In addition to these guidelines, the document *Caractéristiques de la tension fournie par le réseau de transport d'Hydro-Québec*<sup>18</sup> provides information on disturbance levels that may be found on the Hydro-Québec Transmission System.

When assessing the facility's emission levels for harmonic and interharmonic currents, harmonic filter performance must take into account a frequency variation of  $\pm 0.2$  Hz on the Transmission System. Asymmetries generated by the facility's equipment must be added to that.

#### **8.4 EMISSION STUDY FOR INTERHARMONICS**

If Hydro-Québec requires the emission study for interharmonics, it must be carried out:

- Under general conditions, if  $S_{sc\_general}/S_T > 30$
- Under general conditions and under occasional conditions, if  $S_{sc\_general}/S_T < 30$

The emission study for interharmonics must present emission levels that take into account:

- Harmonic impedance loci as supplied by Hydro-Québec

In addition to the results to be presented in the emission study for harmonics in section 7.6, the emission study for interharmonics must present the following results:

- Data for harmonic or interharmonic converter models (using the Thévenin/Norton circuit), where appropriate, and for circuit characteristics (e.g., filters) modeling each source, for interharmonics of the interharmonic orders  $n = 1$  to 49 and all operating conditions
- The maximum interharmonic amplification factor for the interharmonic subgroup of frequencies between 70 Hz and 90 Hz ( $FA_{1+}$ ) as well as the corresponding interharmonic impedance values for the system and facility (amplitudes and angles)
- Tables of results, for interharmonics of the interharmonic orders  $n = 1$  to 49, under general conditions and, if required, under occasional conditions, presenting:

<sup>17</sup> Reference provided for explanatory and information purposes only.

<sup>18</sup> See note 17.

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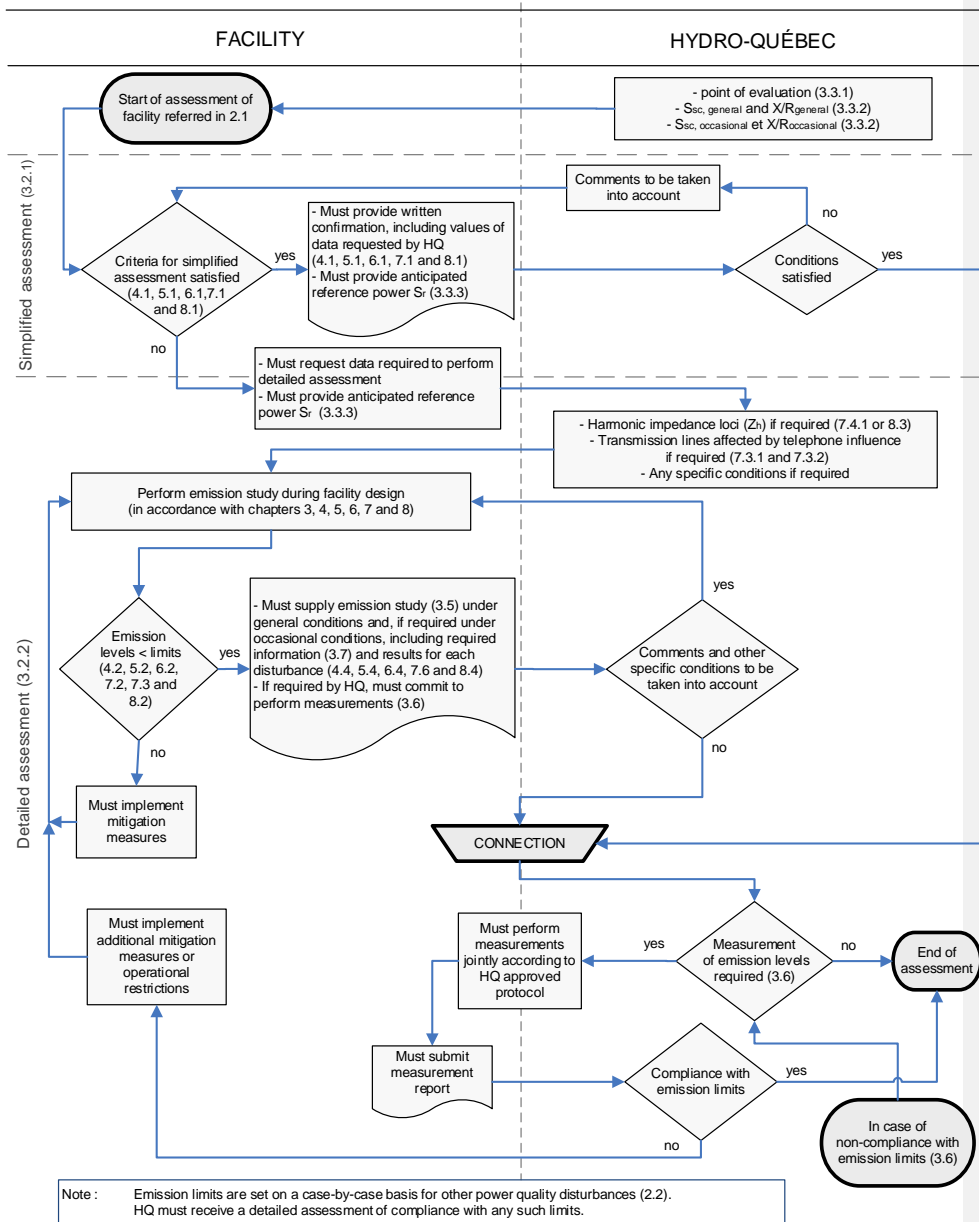
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- Maximum interharmonic currents generated by disturbing equipment within the *facility* under study, along with the respective angular displacements in the presence of multiple equivalent interharmonic current sources
- *Facility* harmonic (and interharmonic) impedance values (amplitudes and angles), including capacitors and filters and the effect of detuning, possible switching operations, etc.
- *System* harmonic (or interharmonic) impedance values that maximize each emission level for harmonic currents, based on *system* harmonic impedance loci
- Maximum emission level for individual interharmonic currents ( $I_{h,n}/I_p$ ), for each interharmonic order

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## Appendix A Required technical information and general procedure for assessing emission limit compliance



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## Appendix B General guidelines for measuring power quality disturbances

General guidelines are provided for measuring power quality *disturbances* covered by the emission limits presented in this document. These guidelines are to be supplemented as needed by a measurement protocol in order to determine emission levels for a given *facility*.

### B.1 Rapid voltage change (RVC)

The RVC is calculated based on consecutive values of the RMS voltage, calculated each second. Each value of the RMS voltage is the quadratic mean of the voltage over a 1 second aggregation interval.

The percent RVC is calculated for a given interval of 9 consecutive seconds according to the equation below:

$$RVC(\%) = \left[ \frac{\max_{9s}(ISV_{3s\ avg}) - \min_{9s}(ISV_{3s\ avg})}{\text{avg}_{9s}(ISV_{3s\ avg})} \right] \times 100$$

Where:

- $ISV_{3s\ avg}$  : Arithmetic mean of three consecutive values of the RMS voltage (each over a 1 second aggregation interval)
- $\max_{9s}(ISV_{3s\ avg})$  : Maximum value of the 7 possible  $ISV_{3s\ avg}$  averages calculated within the 9 second interval
- $\min_{9s}(ISV_{3s\ avg})$  : Minimum value of the 7 possible  $ISV_{3s\ avg}$  averages calculated within the 9 second interval
- $\text{avg}_{9s}(ISV_{3s\ avg})$  : Arithmetic mean of the 7 possible  $ISV_{3s\ avg}$  averages calculated within the 9 second interval preceding the end of the RVC detection interval

A RVC is an intermittent power quality *disturbance*. Assessment of compliance with emission limits is based on forecast maximum values rather than on statistical levels over time.

If the RMS voltage exceeds the voltage dip or the overvoltage threshold during a voltage change, the event is considered to be a voltage dip or an overvoltage rather than a RVC.

### B.2 Flicker

The short-term flicker index ( $P_{st}$ ) is measured over 10-minute aggregation intervals according to standard CAN/CSA-IEC 61000-4-15 [2] and Class A requirements of standard IEC 61000-4-30 [3] adjusted for 120-V lamps.

A measurement protocol is generally required to determine emission levels for flicker.

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Measurements rely on statistical levels over time to assess compliance with emission limits. Compliance is achieved when the 95<sup>th</sup> percentile<sup>19</sup> value of daily recorded emission levels is less than the emission limit and when the 99<sup>th</sup> percentile<sup>20</sup> value is less than 1.25 times this limit.

These statistical values are calculated by discarding flagged data according to standard IEC 61000-4-30 [3] (e.g., voltage dips, temporary overvoltages, momentary interruptions or other interruptions on the system).

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### B.3 Load or current unbalance

The negative-sequence component of the current (or voltage) unbalance is assessed over 10-minute aggregation intervals, in accordance with Class A requirements of standard IEC 61000-4-30 [3].

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A measurement protocol is generally required to determine emission levels for current (or voltage) unbalance.

Measurements rely on statistical levels over time to assess compliance with emission limits. Compliance is achieved when the 95<sup>th</sup> percentile<sup>19</sup> value of daily recorded emission levels is less than the emission limit and when the 99<sup>th</sup> percentile<sup>20</sup> value is less than 1.5 times this limit.

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These statistical values are calculated by discarding flagged data according to standard IEC 61000-4-30 [3] (e.g., voltage dips, temporary overvoltages, momentary interruptions or other interruptions on the system).

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### B.4 Harmonics and interharmonics

Harmonic currents of orders  $n = 2$  to 50 and interharmonic currents of interharmonic orders  $n = 1$  to 49 are measured over 10-minute aggregation intervals according to standard CAN/CSA-IEC 61000-4-7 [1] and Class A requirements of standard IEC 61000-4-30 [3].

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If harmonics are continuously and rapidly fluctuating, the evaluation of emission levels for harmonic currents relies on the group and subgroup method as described in standard CAN/CSA-IEC 61000-4-7 [1].

[With interharmonics, the harmonic level is evaluated using the RMS value of the harmonic group, as defined in standard CAN/CSA IEC 61000-4-7 \[1\].](#)

[The interharmonic level is evaluated using the RMS value of the interharmonic centred subgroup, as defined in standard CAN/CSA IEC 61000-4-7 \[1\].](#)

A measurement protocol is generally required to determine emission levels for harmonic and interharmonic currents.

Measurements rely on statistical levels over time to assess compliance with emission limits. Compliance is achieved when the 95<sup>th</sup> percentile<sup>19</sup> value of daily recorded emission levels is less than the emission limit and when the 99<sup>th</sup> percentile<sup>20</sup> value is less than 1.5 times this limit.

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These statistical values are calculated by discarding flagged data according to standard IEC 61000-4-30 [3] (e.g., voltage dips, temporary overvoltages, momentary interruptions or other interruptions on the system).

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<sup>19</sup> The 95<sup>th</sup> percentile value of daily recorded values is the maximum value obtained when ignoring the top 5% of values recorded during a given day.

<sup>20</sup> The 99<sup>th</sup> percentile value of daily recorded values is the maximum value obtained when ignoring the top 1% of values recorded during a given day.

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## Mandatory reference documents

- [1] Electromagnetic compatibility (EMC) – Part 4-7: Testing and measurement techniques – General guide on harmonics and interharmonics measurements and instrumentation, for power supply systems and equipment connected thereto. National Standard of Canada CAN/CSA-IEC 61000-4-7:13 (R2017).
- [2] Electromagnetic compatibility (EMC) – Part 4-15: Testing and measurement techniques – Flickermeter – Functional and design specifications. National Standard of Canada CAN/CSA-IEC 61000-4-15:12 (R2016).
- [3] Electromagnetic compatibility (EMC) – Part 4-30: Testing and measurement techniques – Power quality measurement methods. [International Standard IEC 61000-4-30:21](#).

The *Transmission Provider* must display on its website a hyperlink pointing to the Canadian Standards Association (CSA) [and International Electrotechnical Commission](#) websites, where it is possible to obtain any copyrighted standard.

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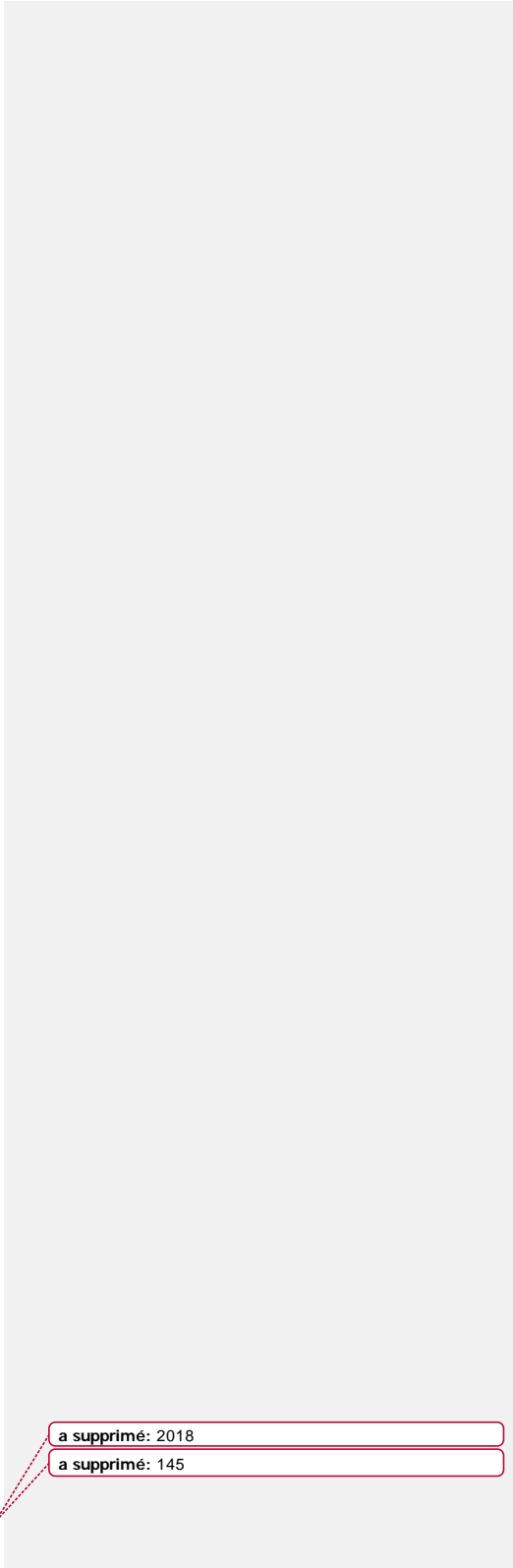
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I hereby certify that the track changes made to the English document (to be filed on February 28, 2022) are a complete and accurate translation of the changes made to the French document (filed on November 30, 2021).



Anna Tomczyk, Certified Translator  
OTTIAQ, Member No. 7979  
Signed in Montréal, Québec, on February 25, 2022